## O<sub>2</sub> Gas Sensor Using Supported Hydrophobic Room-temperature Ionic Liquid Membrane-coated electrode

Rong Wang, Satoshi Hoyano, and Takeo Ohsaka\*

Department of Electronic Chemistry, Interdisciplinary Graduate School of Science and Engineering, Tokyo Institute of Technology, 4259 Nagatsuta, Midori-ku, Yokohama 226-8502

(Received September 16, 2003; CL-030862)

A solid-state amperometric  $O_2$  gas sensor was successfully fabricated by using supported 1-*n*-butyl-3-methylimidazolium hexafluorophosphate (BMIPF<sub>6</sub>) porous polyethylene membrane as a solid-state electrolyte. The present  $O_2$  gas sensor, which is capable of being operated at room temperature, shows a wide detection range and a high stability.

Recently, room-temperature ionic liquids (RTILs) have been used in many areas of chemistry, and may also be useful for fabricating gas sensors,<sup>1</sup> as they have low melting point, wide electrochemical window, and high solubility for a wide range of materials. Especially, a high ionic conductivity of RTIL at room temperature allows the gas sensor to operate at room temperature. In addition, a negligible vapor pressure of RTILs does not cause the drying out of the electrolyte which is a serious problem for the sensors using solid polymer electrolyte films.<sup>2</sup> In this letter, a novel solid-state amperometric O<sub>2</sub> gas sensor based on the supported BMIPF<sub>6</sub> membrane will be proposed.

Figure 1 shows the schematic representation of the electrochemical measurement system used in this study, in which the supported BMIPF<sub>6</sub> membrane was prepared by soaking up the porous polyethylene membrane (7P03A, Teijin Solufill Co., Japan) in BMIPF<sub>6</sub> solution (Fluka) for at least 1 day under reduced pressure at 30 °C. The obtained supported BMIPF<sub>6</sub> membrane was then closely mounted on the surface of the epoxide resin disk, in which a three-electrode system was constructed, to fabricate the O<sub>2</sub> gas-sensing electrode system. The dried pure O<sub>2</sub> (or N<sub>2</sub>) gas, water-saturated pure O<sub>2</sub> (or N<sub>2</sub>) gas and dried O<sub>2</sub>–N<sub>2</sub> gas mixtures used in the electrochemical measurements were introduced through the gas flowing-routes a, b, and c shown in Figure 1, respectively.

The redox behavior of O<sub>2</sub> at the BMIPF<sub>6</sub> membrane-coated electrode is shown in Figure 2. In dried O<sub>2</sub> atmosphere, a couple of redox peaks were observed on the CV (voltammogram (b)) with formal potential at ca. -0.66 V vs Ag, which is similar to that obtained for O<sub>2</sub> reduction in BMIPF<sub>6</sub> solution.<sup>3</sup> Thus, the observed cathodic and anodic peaks can be assigned to the one-electron reduction of  $O_2$  to superoxide ion  $(O_2^{-1})$  and the reoxidation of O2-\* to O2, respectively. This well-defined CV also indicates that the supported BMIPF<sub>6</sub> membrane has a high ionic conductivity at room temperature. In water-saturated O2 atmosphere (voltammogram (c)), the cathodic peak potential shifted positively and the cathodic peak current value increased about twice compared with that obtained in dried O<sub>2</sub> atmosphere. Thus, the new cathodic peak at about -0.7 V can be assigned to the two-electron reduction of  $O_2$  to  $H_2O_2$ .<sup>4</sup> In addition, the anodic peak at ca. -0.53 V disappeared and two new anodic peaks at 0.35 V and ca. 1.0 V were observed. These two new anodic



**Figure 1.** Schematic representation of the electrochemical measurement system used in this study. (1)  $N_2$  gas tank, (2)  $O_2$  gas tank, (3) gas blender, (4) valve, (5) bottle containing Milli-Q water, (6) supported BMIPF<sub>6</sub> membrane, (7) GC disk (diameter: 1 mm) working electrode, (8) Ag disk (diameter: 1 mm) reference electrode, (9) Pt ring (width: 1 mm, length: 50 mm) counter electrode, (10) epoxide resin, (11)  $O_2$  gas-sensing electrode system, (12) potentiostat and (13) computer.



**Figure 2.** Cyclic voltammograms (CVs) obtained at the supported BMIPF<sub>6</sub> membrane-coated electrode at  $25 \pm 1$  °C under (a) dried N<sub>2</sub> gas, (b, d) dried O<sub>2</sub> gas, and (c) water-saturated O<sub>2</sub> gas atmospheres. After measuring voltammogram (c), the electrode system was held in dried O<sub>2</sub> gas atmosphere for 3 min, and then voltammogram (d) was obtained. Voltammogram (e) was obtained at supported EMIBF<sub>4</sub> membrane-coated electrode under dried O<sub>2</sub> atmosphere. Scan rate was  $100 \text{ mV s}^{-1}$ .

peaks can be regarded as the reoxidation of  $H_2O_2$ . After measuring voltammogram (c), the electrode system was held in dried  $O_2$  gas atmosphere for 3 min, and then the voltammogram (d) was obtained. The voltammogram (d) slightly negatively shifted compared with voltammogram (b), probably due to the potential change of the Ag quasi-reference electrode. The repeated intro-

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duction and removal of moisture resulted in the reproducible voltammograms of (c) and (d), respectively. Thus, we found that the water contained in the O<sub>2</sub>-sensing electrode system changed the reduction of O<sub>2</sub> from one-electron reaction to two-electron reaction, but the water in the electrode system could be easily removed by holding the electrode system in dried O<sub>2</sub> gas atmosphere for ca. 3 min (Figure 2), and thus, the electrode system can be recovered as a result of the fact that the solid-state electrolyte membrane was composed of the hydrophobic materials, i.e., BMIPF<sub>6</sub><sup>4</sup> and porous polyethylene membrane. Figure 2 also shows the CV (voltammogram (e)) obtained at 1-ethyl-3-methylimidazolium tetrafluoroborate (EMIBF<sub>4</sub>) membrane-coated electrode in dried O<sub>2</sub> atmosphere. As EMIBF<sub>4</sub> is a hydrophilic ionic liquid, compared with BMIPF<sub>6</sub>, the saturated concentration of O<sub>2</sub> in the supported EMIBF<sub>4</sub> membrane is lower and consequently the smaller redox response was obtained at the EMIBF<sub>4</sub> membrane-coated electrode (voltammograms (b) and (e)).

Potential-step chronoamperometry was used to characterize the supported  $BMIPF_6$  membrane-coated electrode system as an



**Figure 3.** Typical potential-step chronoamperometric current responses obtained at the supported BMIPF<sub>6</sub> membrane-coated electrode in dried O<sub>2</sub> gas streams at  $25 \pm 1$  °C. O<sub>2</sub> concentration was changed from 0 to 100% (v/v) O<sub>2</sub> in O<sub>2</sub>–N<sub>2</sub> gas mixtures. The potential step was repeated between 0 and -0.9 V vs Ag every 20 s, shown as the inset. *t*<sub>c</sub> and *t*<sub>a</sub> mean the sampling times during the cathodic and anodic potential steps, respectively.



**Figure 4.** Variation of the current signal with  $O_2$  concentration in  $O_2$ - $N_2$  gas mixed streams at the supported BMIPF<sub>6</sub> membrane-coated electrode. The data were obtained from Figure 3. The current responses were recorded at (a)  $t_c$ : 0.4 s, (b)  $t_c$ : 20 s, and (c)  $t_a$ : 0.4 s.

O<sub>2</sub> gas sensor. The potential-time waveform of potential-step chronoamperometry and chronoamperometric current responses obtained for different concentrations of O<sub>2</sub> in gas phase are shown in Figure 3. When the potential was stepped from 0 to -0.9 V, the O<sub>2</sub> molecule in the supported BMIPF<sub>6</sub> membrane was reduced to  $O_2^{-}$ , and after several seconds the reduction current attained an approximately constant value, as a steadystate supply of  $O_2$  from the gas phase into the membrane can be reached. In the reverse step (from -0.9 to 0 V), the current corresponding to the reoxidation of  $O_2^{-}$  to  $O_2$  was observed. Unlike the reduction current, the oxidation current gradually decreased and reached the background level after 20 s, because  $O_2^{-1}$  in the membrane was completely consumed. Thus, the transient and steady-state currents for the reduction of  $O_2$  to  $O_2^{-1}$  $(I_{c,trans} \text{ and } I_{c,s} \text{ obtained at } 0.4 \text{ and } 20 \text{ s after the potential was}$ stepped to -0.9 V) as well as the transient current corresponding to the reoxidation of  $O_2^{-}$  to  $O_2$  ( $I_{a,trans}$  obtained at 0.4 s after the potential was stepped to 0 V) were typically used for measuring the concentration of  $O_2$  in gas phase. The calibration curves (Figure 4) obtained for  $I_{c,s}$  and  $I_{c,trans}$  showed the straight lines with the sensitivities of 0.80 and 4.60  $\mu$ A (% (v/v))<sup>-1</sup>, respectively. The good linearity  $(r^2 > 0.998)$  of these two calibration curves obtained in the O<sub>2</sub> concentration range from 0 to 100% (v/v) demonstrates that this  $O_2$  gas sensor has a wide detection range. The calibration curve obtained for Ia,trans could be expressed by a quadratic equation, probably resulting from the limited diffusion of  $O_2^{-}$  in the membrane and its decomposition. This point remains to be clarified theoretically. Ic,trans response is recommended to use for O<sub>2</sub> sensing, as it is simpler to use a linear current-concentration relationship rather than a quadratic one, and in addition the  $I_{c,trans}$  response is larger than the  $I_{c,s}$  response. The utility of the present O<sub>2</sub> sensor is restricted for detecting  $O_2$  in a dry gas stream. The sensor can be continuously used for at least twelve hours, and it can be easily recovered even if a water-containing sample gas should be flowed through the electrode system.

In conclusion, we have successfully developed an amperometric O<sub>2</sub> gas sensor based on the supported BMIPF<sub>6</sub> porous polyethylene membrane-coated electrodes. Some characteristic currents i.e.,  $I_{c,trans}$ ,  $I_{c,s}$ , and  $I_{a,trans}$ , obtained by potential-step chronoamperometry were used for determining the O<sub>2</sub> concentration in a dry gas stream. This sensor showed a wide detection range, a high sensitivity and a good reproducibility.

The authors gratefully acknowledge Teijin Solufill Co. for supplying the porous polyethylene membrane and Dr. Okajima for his helpful discussion. The present work was financially supported by Grant-in-Aids for Scientific Research on Priority Areas (No. 417) and Scientific Research (A) (No. 10305064) from the Ministry of Education, Culture, Sports, Science and Technology, Japan. R. W. acknowledges the government of Japan for a Monbu-Kagakusho scholarship.

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